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Formerly Utilized Sites Remedial Action Program (FUSRAP)  
Contract No. DE-AC05-81OR20722

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**RADIOLOGICAL CHARACTERIZATION  
REPORT FOR THE RESIDENTIAL  
PROPERTY AT 5 HANCOCK STREET**

**Lodi, New Jersey**

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September 1989



Bechtel National, Inc.

063982

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SEP 29 1989

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Attention: Robert G. Atkin  
Technical Services Division

Subject: Bechtel Job No. 14501, FUSRAP Project  
DOE Contract No. DE-AC05-81OR20722  
Publication of Radiological Characterization Report  
for seventeen residential properties, four municipal  
properties, and seven commercial properties in  
Lodi and Maywood, New Jersey  
Code: 7315/WBS: 138

Dear Mr. Atkin:

Enclosed is one copy each of the 28 subject published reports  
for the properties listed in Attachment 1. These reports  
incorporate all comments received in this review cycle (CCNs  
063165, 063327, 062285, and 061568) and are being published with  
approval of Steve Oldham, as reported in CCN 063868.

Also enclosed (as Attachment 2) is a proposed distribution list  
for these reports. Please send us any changes to the proposed  
distribution list at your earliest convenience so we may  
distribute the reports.

BNI would like to express our thanks to Mr. Oldham for his  
cooperation and efforts to review these drafts in an accelerated  
manner. His efforts have allowed us to publish these reports on  
schedule. If you have any questions about these documents,  
please call me at 576-4718.

Very truly yours,

R. C. Robertson  
Project Manager - FUSRAP

RCR:wfs:1756x  
Enclosure: As stated

cc: J. D. Berger, ORAU (w/e)  
N. J. Beskid, ANL (w/e)

CONCURRENCE

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RADIOLOGICAL CHARACTERIZATION REPORT  
FOR THE RESIDENTIAL PROPERTY AT  
5 HANCOCK STREET  
LODI, NEW JERSEY

SEPTEMBER 1989

Prepared for

UNITED STATES DEPARTMENT OF ENERGY  
OAK RIDGE OPERATIONS OFFICE  
Under Contract No. DE-AC05-81OR20722

By

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## ABBREVIATIONS

cm	centimeter
cm <sup>2</sup>	square centimeter
cpm	counts per minute
dpm	disintegrations per minute
ft	foot
h	hour
in.	inch
km <sup>2</sup>	square kilometer
L	liter
L/min	liters per minute
m	meter
m <sup>2</sup>	square meter
MeV	million electron volts
μR/h	microroentgens per hour
mi	mile
mi <sup>2</sup>	square mile
min	minute
mrad/h	millirad per hour
mrem	millirem
mrem/yr	millirem per year
pCi/g	picocuries per gram
pCi/L	picocuries per liter
WL	working level
yd	yard
yd <sup>3</sup>	cubic yard

## 1.0 INTRODUCTION AND SUMMARY

This section provides a brief description of the history and background of the Maywood site and its vicinity properties. Data obtained from the radiological characterization of this vicinity property are also presented.

### 1.1 INTRODUCTION

The 1984 Energy and Water Appropriations Act authorized the U.S. Department of Energy (DOE) to conduct a decontamination research and development project at four sites, including the site of the former Maywood Chemical Works (now owned by the Stepan Company) and its vicinity properties. The work is being administered under the Formerly Utilized Sites Remedial Action Program (FUSRAP) under the direction of the DOE Division of Facility and Site Decommissioning Projects. Several residential, commercial, and municipal properties in Lodi, New Jersey, are included in FUSRAP as vicinity properties. Figure 1-1 shows the location of the Lodi vicinity properties in relation to the former Maywood Chemical Works.

The U.S. Government initiated FUSRAP in 1974 to identify, clean up, or otherwise control sites where low-activity radioactive contamination (exceeding current guidelines) remains from the early years of the nation's atomic energy program or from commercial operations that resulted in conditions Congress has mandated that DOE remedy (Ref. 1).

FUSRAP is currently being managed by DOE Oak Ridge Operations. As the Project Management Contractor for FUSRAP, Bechtel National, Inc. (BNI) is responsible to DOE for planning, managing, and implementing FUSRAP.

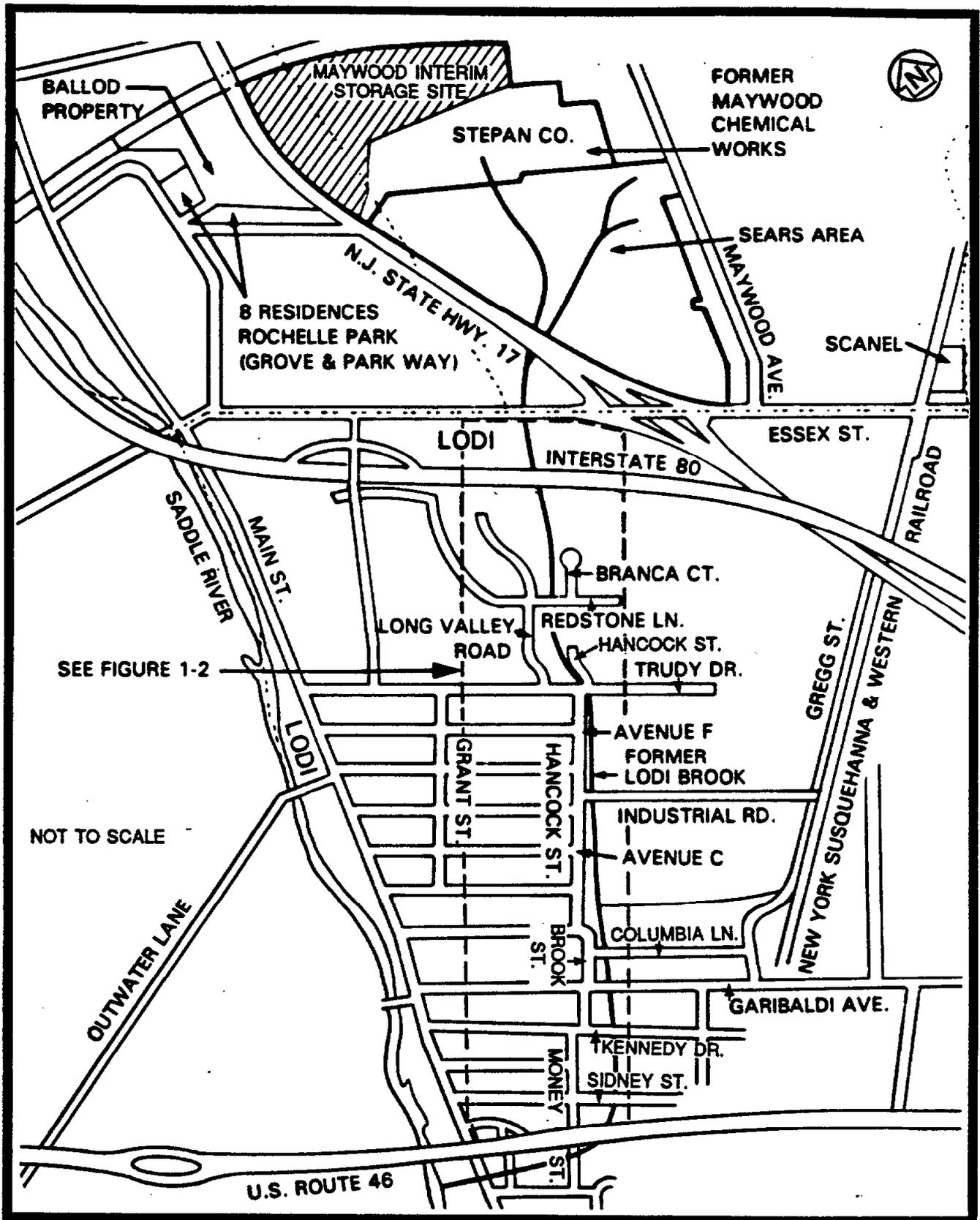


FIGURE 1-1 LOCATION OF LODI VICINITY PROPERTIES

## 1.2 PURPOSE

The purpose of the 1986 survey performed by BNI was to locate the horizontal and vertical boundaries of radionuclide concentrations exceeding remedial action guidelines.

## 1.3 SUMMARY

This report details the procedures and results of the radiological characterization of the property at 5 Hancock Street (Figure 1-2) in Lodi, New Jersey, which was conducted in November and December 1986. Additional data was obtained in November and December 1988.

Ultimately, the data generated during the radiological characterization will be used to define the complete scope of remedial action necessary to release the site.

This characterization confirmed that thorium-232 is the primary radioactive contaminant at this property. Results of surface soil samples for 5 Hancock Street showed maximum concentrations of thorium-232 and radium-226 to be 5.8 and 2.9 pCi/g, respectively. The maximum concentration of uranium-238 in surface soil samples was less than 13.8 pCi/g.

Subsurface soil sample concentrations ranged from 1.0 to 7.4 pCi/g for thorium-232 and from 0.7 to 1.7 pCi/g for radium-226. The average background level in this area for both radium-226 and thorium-232 is 1.0 pCi/g. The concentrations of uranium-238 in subsurface soil samples ranged from 1.0 to less than 13.3 pCi/g. Because the major contaminants at the vicinity properties are thorium and radium, the decontamination guidelines provide the appropriate guidance for the cleanup activities. DOE

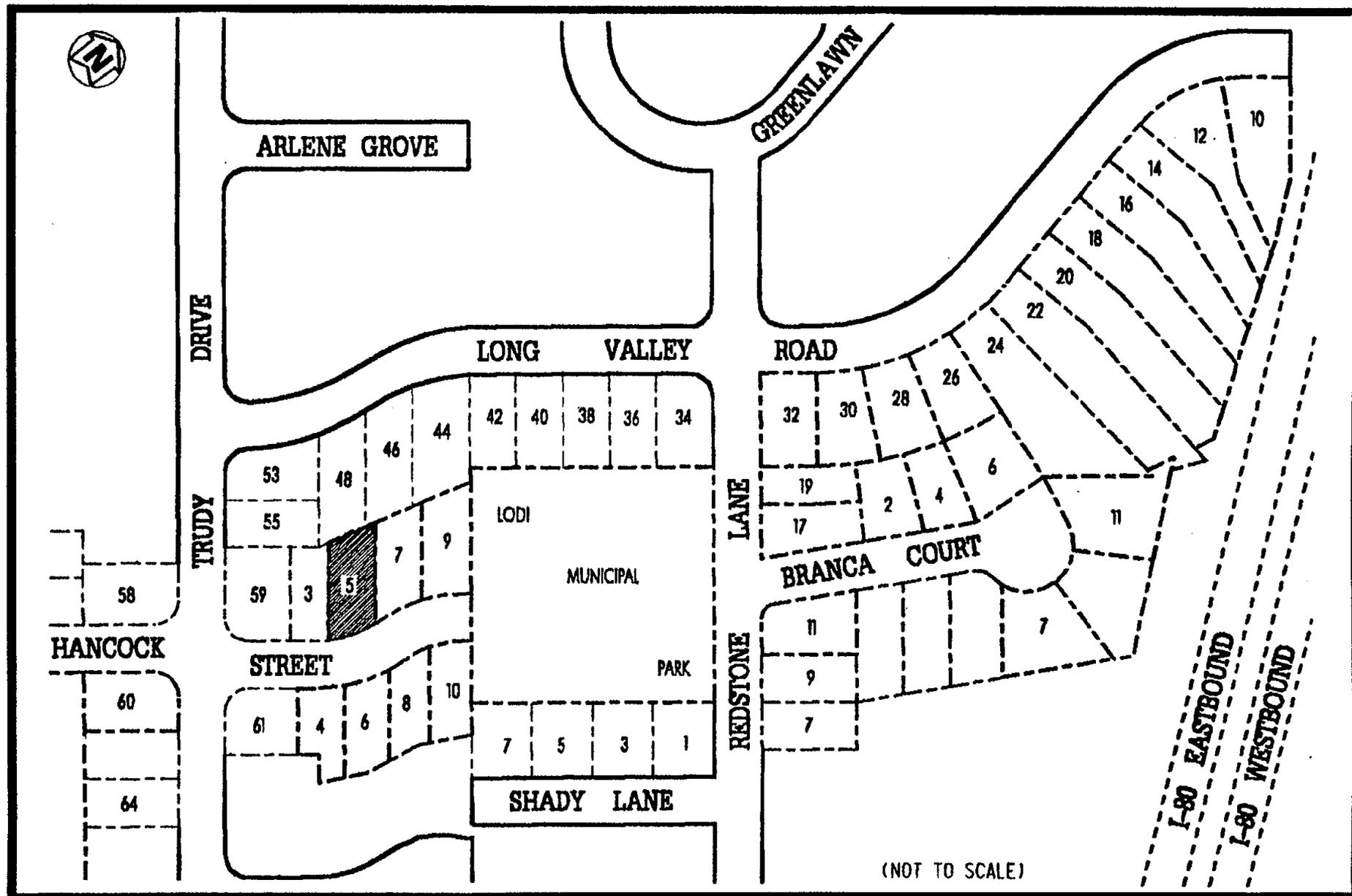


FIGURE 1-2 LOCATION OF 5 HANCOCK STREET

believes that these guidelines are conservative for considering potential adverse health effects that might occur in the future from any residual contamination. The dose contributions from uranium and any other radionuclides not numerically specified in these guidelines are not expected to be significant following decontamination. In addition, the vicinity properties will be decontaminated in a manner so as to reduce future doses to levels that are as low as reasonably achievable (ALARA) (Ref. 2).

Soil analysis data for this property did not indicate surface contamination. Subsurface investigation by gamma logging indicated contamination to a depth of 0.76 m (2.5 ft).

Exterior gamma radiation exposure rates ranged from 9 to 13  $\mu\text{R/h}$ , including background. The indoor measurement showed a rate of 6  $\mu\text{R/h}$ , including background.

The radon-222 measurements inside the residence indicated concentrations of 0.2 and 0.4 pCi/L, respectively, which are within the DOE guideline of 3.0 pCi/L.

Measurements for radon daughters ranged from 0.0005 to 0.003 working level (WL), and measurements for thoron daughters ranged from 0.0007 to 0.003 WL.

All data tables for this property appear at the end of this report.

#### 1.4 CONCLUSIONS

Evaluation of data collected, analyses performed, and historical documentation reviewed indicates the presence of radiological contamination on the property located at 5 Hancock Street. This contamination is primarily subsurface contamination ranging from a depth of 0.30 m (1.0 ft) to 0.76 m (2.5 ft). In addition, the contamination appears to extend beneath the back porch of the residence as well as beneath an above-ground pool in the backyard. The total affected area is estimated to be approximately 25 percent of the property. These conclusions are supported by documentation that establishes the presence of the former channel of Lodi Brook in this area. This channel is the suspected transport mechanism for the radiological contamination.

## 2.0 SITE HISTORY

The Maywood Chemical Works was founded in 1895. The company began processing thorium from monazite sand in 1916 (during World War I) for use in manufacturing gas mantles for various lighting devices. The company continued this work until 1956. Process wastes from manufacturing operations were pumped to two areas surrounded by earthen dikes on property west of the plant. Subsequently, some of the contaminated wastes migrated onto adjacent and vicinity properties.

In 1928 and again between 1944 and 1946, some of the residues from the processing operations were moved from the company's property and used as mulch and fill in nearby low-lying areas. The fill material consisted of tea and coca leaves mixed with other material resulting from operations at the plant. Some fill material apparently contained thorium process wastes (Ref. 3).

Uncertainty exists as to how the properties in Lodi were contaminated. According to an area resident, fill from an unknown source was brought to Lodi and spread over large portions of the previously low-lying and swampy area. For several reasons, however, a more plausible explanation is that the contamination migrated along a drainage ditch originating on the Maywood Chemical Works property. First, it can be seen from photographs and tax maps of the area that the course of a previously existing stream known as Lodi Brook, which originated at the former Maywood Chemical Works, generally coincides with the path of contamination in Lodi. The brook was subsequently replaced by a storm drain system as the area was developed. Second, samples taken from Lodi properties indicate elevated concentrations of a series of elements known as rare earths. Rare earth elements are

typically found in monazite sands, which also contain thorium. This type of sand was feedstock at the Maywood Chemical Works, and elevated levels are known to exist in the by-product of the extraction process. Third, the ratio of thorium to other radionuclides found on these Lodi properties is comparable to the ratio found in contaminated material on other properties in Lodi (Ref. 4). And finally, long-time residents of Lodi recalled chemical odors in and around the brook in Lodi and steam rising off the water. These observations suggest that discharges of contaminants occurred upstream.

The Stepan Chemical Company (now called the Stepan Company) purchased Maywood Chemical Works in 1959. The Stepan Company itself has never been involved in the manufacture or processing of any radioactive materials (Ref. 5).

## 2.1 PREVIOUS RADIOLOGICAL SURVEYS

Numerous surveys of the Maywood site and its vicinity properties have been conducted. Among the past surveys, three that are pertinent to this vicinity property are detailed in this section.

January 1981--The Nuclear Regulatory Commission (NRC) directed that a survey be conducted of the Stepan Company property and its vicinity properties in January 1981. Using the Stepan Company plant as the center, a 10.3-km<sup>2</sup> (4-mi<sup>2</sup>) aerial survey was conducted by the EG&G Energy Measurements Group, which identified anomalous concentrations of thorium-232 to the north and south of the Stepan Company property. The Lodi vicinity properties were included in this survey (Ref. 6).

June 1984--In June 1984, Oak Ridge National Laboratory (ORNL) conducted a "drive-by" survey of Lodi using its "scanning van." Although not comprehensive, the survey indicated areas requiring further investigation (Ref. 7).

September 1986--At the request of DOE, ORNL conducted radiological surveys of the vicinity properties in Lodi in September 1986 to determine which properties contained radioactive contamination in excess of DOE guidelines and would, therefore, require remedial action (Ref. 8).

## 2.2 REMEDIAL ACTION GUIDELINES

Table 2-1 summarizes the DOE guidelines for residual contamination. The thorium-232 and radium-226 limits listed in Table 2-1 will be used to determine the extent of remedial action required at the vicinity properties. DOE developed these guidelines to be consistent with the guidelines established by the U.S. Environmental Protection Agency (EPA) for the Uranium Mill Tailings Remedial Action Program.

**TABLE 2-1**  
**SUMMARY OF RESIDUAL CONTAMINATION GUIDELINES**

**BASIC DOSE LIMITS**

The basic limit for the annual radiation dose received by an individual member of the general public is 100 mrem/yr.

**SOIL GUIDELINES**

<u>Radionuclide</u>	<u>Soil Concentration (pCi/g) Above Background<sup>a,b,c</sup></u>
Radium-226 Radium-228 Thorium-230 Thorium-232	5 pCi/g when averaged over the first 15 cm of soil below the surface; 15 pCi/g when averaged over any 15-cm-thick soil layer below the surface layer.
Other Radionuclides	Soil guidelines will be calculated on a site-specific basis using the DOE manual developed for this use.

**STRUCTURE GUIDELINES**

**Airborne Radon Decay Products**

Generic guidelines for concentrations of airborne radon decay products shall apply to existing occupied or habitable structures on private property that has no radiological restrictions on its use; structures that will be demolished or buried are excluded. The applicable generic guideline (40 CFR 192) is: In any occupied or habitable building, the objective of remedial action shall be, and reasonable effort shall be made to achieve, an annual average (or equivalent) radon decay product concentration (including background) not to exceed 0.02 WL<sup>d</sup>. In any case, the radon decay product concentration (including background) shall not exceed 0.03 WL. Remedial actions are not required in order to comply with this guideline when there is reasonable assurance that residual radioactive materials are not the cause.

**External Gamma Radiation**

The average level of gamma radiation inside a building or habitable structure on a site that has no radiological restrictions on its use shall not exceed the background level by more than 20 µR/h.

**Indoor/Outdoor Structure Surface Contamination**

<u>Radionuclide<sup>f</sup></u>	<u>Allowable Surface Residual Contamination<sup>g</sup></u> (dpm/100 cm <sup>2</sup> )		
	<u>Average<sup>g,h</sup></u>	<u>Maximum<sup>h,i</sup></u>	<u>Removable<sup>h,j</sup></u>
Transuranics, Ra-226, Ra-228, Th-230, Th-228 Pa-231, Ac-227, I-125, I-129	100	300	20
Th-Natural, Th-232, Sr-90, Ra-223, Ra-224 U-232, I-126, I-131, I-133	1,000	3,000	200
U-Natural, U-235, U-238, and associated decay products	5,000 α	15,000 α	1,000 α
Beta-gamma emitters (radionuclides with decay modes other than alpha emission or spontaneous fission) except Sr-90 and others noted above	5,000 β - γ	15,000 β - γ	1,000 β - γ

**TABLE 2-1  
(CONTINUED)**

<sup>a</sup>These guidelines take into account ingrowth of radium-226 from thorium-230 and of radium-228 from thorium-232, and assume secular equilibrium. If either thorium-230 and radium-226 or thorium-232 and radium-228 are both present, not in secular equilibrium, the guidelines apply to the higher concentration. If other mixtures of radionuclides occur, the concentrations of individual radionuclides shall be reduced so that 1) the dose for the mixtures will not exceed the basic dose limit, or 2) the sum of ratios of the soil concentration of each radionuclide to the allowable limit for that radionuclide will not exceed 1 ("unity").

<sup>b</sup>These guidelines represent allowable residual concentrations above background averaged across any 15-cm-thick layer to any depth and over any contiguous 100-m<sup>2</sup> surface area.

<sup>c</sup>Localized concentrations in excess of these limits are allowable, provided that the average concentration over a 100-m<sup>2</sup> area does not exceed these limits. In addition, every reasonable effort shall be made to remove any source of radionuclide that exceeds 30 times the appropriate soil limit, regardless of the average concentration in the soil.

<sup>d</sup>A working level (WL) is any combination of short-lived radon decay products in 1 liter of air that will result in the ultimate emission of  $1.3 \times 10^5$  MeV of potential alpha energy.

<sup>e</sup>As used in this table, dpm (disintegrations per minute) means the rate of emission by radioactive material as determined by correcting the counts per minute observed by an appropriate detector for background, efficiency, and geometric factors associated with the instrumentation.

<sup>f</sup>Where surface contamination by both alpha- and beta-gamma-emitting radionuclides exists, the limits established for alpha- and beta-gamma-emitting radionuclides should apply independently.

<sup>g</sup>Measurements of average contamination should not be averaged over more than 1 m<sup>2</sup>. For objects of less surface area, the average shall be derived for each such object.

<sup>h</sup>The average and maximum radiation levels associated with surface contamination resulting from beta-gamma emitters should not exceed 0.2 mrad/h and 1.0 mrad/h, respectively, at 1 cm.

<sup>i</sup>The maximum contamination level applies to an area of not more than 100 cm<sup>2</sup>.

<sup>j</sup>The amount of removable radioactive material per 100 cm<sup>2</sup> of surface area should be determined by wiping that area with dry filter or soft absorbent paper, applying moderate pressure, and measuring the amount of radioactive material on the wipe with an appropriate instrument of known efficiency. When removable contamination on objects of surface area less than 100 cm<sup>2</sup> is determined, the activity per unit area should be based on the actual area and the entire surface should be wiped. The numbers in this column are maximum amounts.

### 3.0 HEALTH AND SAFETY PLAN

BNI is responsible for protecting the health of personnel assigned to work at the site. As such, all subcontractors and their personnel were required to comply with the provisions of BNI health and safety requirements and as directed by the on-site BNI Health and Safety Officer.

#### 3.1 SUBCONTRACTOR TRAINING

Before the start of work, all subcontractor personnel attended an orientation session presented by the BNI Health and Safety Officer to explain the nature of the material to be encountered in the work and the personnel monitoring and safety measures that are required.

#### 3.2 SAFETY REQUIREMENTS

Subcontractor personnel complied with the following BNI requirements:

- o Bioassay--Subcontractor personnel submitted bioassay samples before or at the beginning of on-site activity, upon completion of the activity, and periodically during site activities as requested by BNI.
- o Protective Clothing/Equipment--Subcontractor personnel were required to wear the protective clothing/equipment specified in the subcontract or as directed by the BNI Health and Safety Officer.
- o Dosimetry--Subcontractor personnel were required to wear and return daily the dosimeters and monitors issued by BNI.
- o Controlled Area Access/Egress--Subcontractor personnel and equipment entering areas where access and egress were controlled for radiation and/or chemical safety purposes were surveyed by the BNI Health and Safety Officer (or personnel representing BNI) for contamination before leaving those areas.

- o Medical Surveillance--Upon written direction from BNI, subcontractor personnel who work in areas where hazardous chemicals might exist were given a baseline and periodic health assessment defined in BNI's Medical Surveillance Program.

Radiation and/or chemical safety surveillance of all activities related to the scope of work was under the direct supervision of personnel representing BNI.

Health and safety-related requirements for all activities involving exposure to radiation, radioactive material, chemicals, and/or chemically contaminated materials and other associated industrial safety hazards are generated in compliance with applicable regulatory requirements and industry-wide standards. Copies of these requirements are located at the BNI project office for use by project personnel.

## 4.0 CHARACTERIZATION PROCEDURES

A master grid was established by the surveyor. BNI's radiological support subcontractor, Thermo Analytical/Eberline (TMA/E), established a grid on individual properties. The size of the grid blocks was adjusted to characterize each property adequately. The grid origin allows the grid to be reestablished during remedial action and is correlated with the New Jersey state grid system. All data correspond to coordinates on the characterization grid. The grid with the east and north coordinates is shown on all figures included in Sections 4.0 and 5.0 of this report.

### 4.1 FIELD RADIOLOGICAL CHARACTERIZATION

This section provides a description of the instrumentation and methodologies used to obtain exterior surface and subsurface measurements during radiological characterization of this project.

#### 4.1.1 Measurements Taken and Methods Used

An initial walkover survey was performed using an unshielded gamma scintillation detector [5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide probe] to identify areas of elevated radionuclide activity. Near-surface gamma measurements taken using a cone-shielded gamma scintillation detector were also used to determine areas of surface contamination. The shielded detector ensured that the majority of the radiation detected by the instrument originated from the ground directly beneath the unit. Shielding against lateral gamma flux, or shine, from nearby areas of contamination minimized potential sources of error in the measurements. The measurements were taken 30.4 cm (12 in.) above the ground at the intersections of

3.0-m (10-ft) grid lines. The shielded detector was calibrated at the Technical Measurements Center (TMC) in Grand Junction, Colorado, to provide a correlation of counts per minute (cpm) to picocuries per gram (pCi/g). This calibration demonstrated that approximately 11,000 cpm corresponds to the DOE guideline of 5 pCi/g plus local average background of 1 pCi/g for thorium-232 in surface soils (Ref. 9).

A subsurface investigation was conducted to determine the depth to which the previously identified surface contamination extended and to locate subsurface contamination where there was no surface manifestation. The subsurface characterization consisted of drilling nine boreholes (Figure 4-1) [using either a 7.6-cm- (3-in.-) or 15.2-cm- (6-in.-) diameter auger bit], and gamma logging them. The boreholes were drilled to depths determined in the field by the radiological and geological support representatives.

The downhole gamma logging technique was used because the procedure can be accomplished in less time than collecting soil samples, and the need for analyzing these samples in a laboratory is eliminated. A 5.0- by 5.0-cm (2- by 2-in.) sodium iodide gamma scintillation detector was used to perform the downhole logging. The instrument was calibrated at TMC where it was determined that a count rate of approximately 40,000 cpm corresponds to the 15-pCi/g subsurface contamination guideline for thorium-232. This relationship has also been corroborated by results from previous characterizations where thorium-232 was found (Ref. 9).

Gamma radiation measurements were taken at 15.2-cm (6-in.) vertical intervals to determine the depth and concentration of the contamination. The gamma-logging data were reviewed

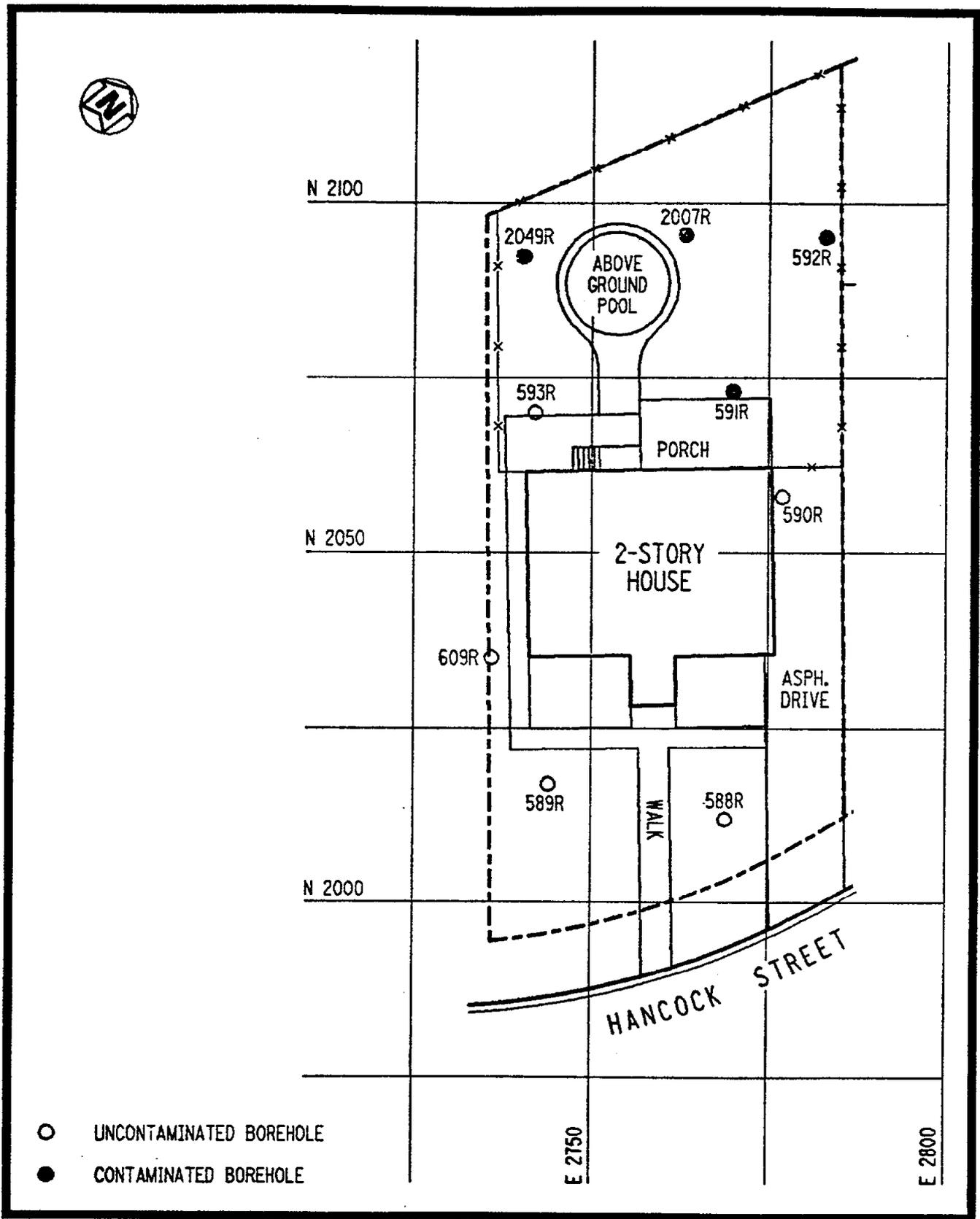


FIGURE 4-1 BOREHOLE LOCATIONS AT 5 HANCOCK STREET

to identify trends, whether or not concentrations exceeded the guidelines.

#### 4.1.2 Sample Collection and Analysis

To identify surface areas where the level of contamination exceeded the DOE guideline of 5 pCi/g for thorium-232, areas with measurements of more than 11,000 cpm were plotted. Using these data as well as data from previous surveys (Refs. 5, 6, 7, and 8), the locations of biased surface soil samples were selected to better define the limits of contamination. Surface soil samples were taken at nine locations (Figure 4-2) and analyzed for thorium-232, uranium-238, and radium-226. Each sample was dried, pulverized, and counted for 10 min using an intrinsic germanium detector housed in a lead counting cave lined with cadmium and copper. The pulse height distribution was sorted using a computer-based, multichannel analyzer. Radionuclide concentrations were determined by comparing the gamma spectrum of each sample with the spectrum of a certified counting standard for the radionuclide of interest.

Subsurface soil samples were collected from nine locations (Figure 4-2) using either the side-wall sampling method or a 7.6-cm (3.0-in.) outside diameter (O.D.) split-spoon sampler. Samples were analyzed to compare laboratory soil sample results to downhole gamma radiation measurements. The side-wall method utilized a cup or can attached to a steel pipe or wooden stake, which was inserted into the borehole and used to scrape samples off the side of the borehole at a specified depth. The subsurface soil samples were analyzed for radium-226, uranium-238, and thorium-232 in the same manner as the surface soil samples.

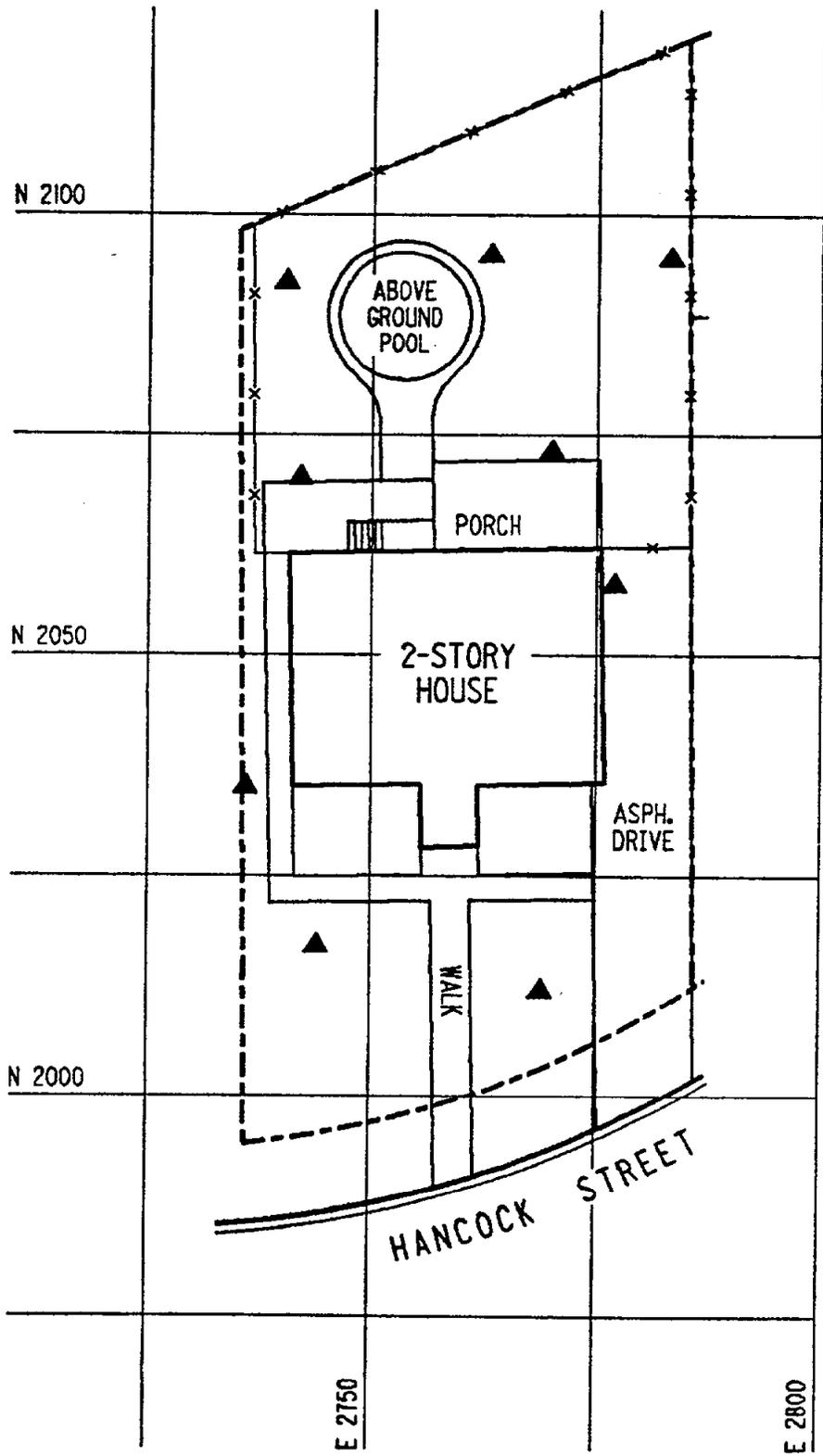


FIGURE 4-2 SURFACE AND SUBSURFACE SOIL SAMPLING LOCATIONS AT 5 HANCOCK STREET

#### 4.2 BUILDING RADIOLOGICAL CHARACTERIZATION

After evaluating previous radiological survey data as well as data from this characterization, it was suspected that contamination might be present under the foundation of the residence. A radon measurement was obtained to verify the presence of contaminated material under the residence and to estimate potential occupational exposures during future remedial actions.

Indoor radon measurements were made using the Tedlar bag method. Samples were collected by pumping air into a Tedlar bag at a rate of approximately 2 L/min. The air sample was transferred directly into a scintillation cell with an interior coating of zinc sulfide and an end window for viewing the scintillations. Analysis of the sample was simplified by allowing the radon decay products to build up over time. This method allowed all the radon decay products to come into secular equilibrium with the radon. The scintillation cell was placed in contact with a photomultiplier tube, and the scintillations were counted using standard nuclear counting instrumentation.

Indoor air samples were collected to determine a WL for radon and thoron daughters. To measure radon daughters, an air sample was collected for exactly 5 min through a 0.45-micron filter at a rate of 11 L/min for a total sample volume of 55 L. Alpha particle activity on the filter paper was counted from 40 to 90 min after sampling. An alpha scintillation detector coupled to a count-rate meter or digital scaler was used. Measurements for thoron daughters were made using the same method as for radon daughters with the exception of the time between collection of the air sample and counting of the alpha particle activity. In the case of thoron daughters, the sample was allowed to age for

at least 5 h after sampling before alpha activity was counted. This elapsed time allowed radon daughters, which may have been present with the thoron daughters, to decay sufficiently so as not to interfere in calculating the WL for thoron daughters.

Exterior gamma exposure rate measurements were made at six locations throughout the property grid system and at one location inside the residence. To obtain these measurements, either a 5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide gamma scintillation detector designed to detect gamma radiation only or a pressurized ionization chamber (PIC) was used. Measurement locations are shown in Figure 4-3. The PIC instrument has a response to gamma radiation that is proportional to exposure in roentgens. A conversion factor for gamma scintillation to the PIC was established through a correlation of these two measurements at four locations in the vicinity of the property. The unshielded gamma scintillation detector readings were then used to estimate gamma exposure rates for each location. These measurements were taken 1 m (3 ft) above the ground. The locations were determined to be representative of the entire property. Interior measurements are generally obtained with the gamma scintillation instrument rather than the PIC because of its smaller size and the desire to minimize the technician's time inside the residence.

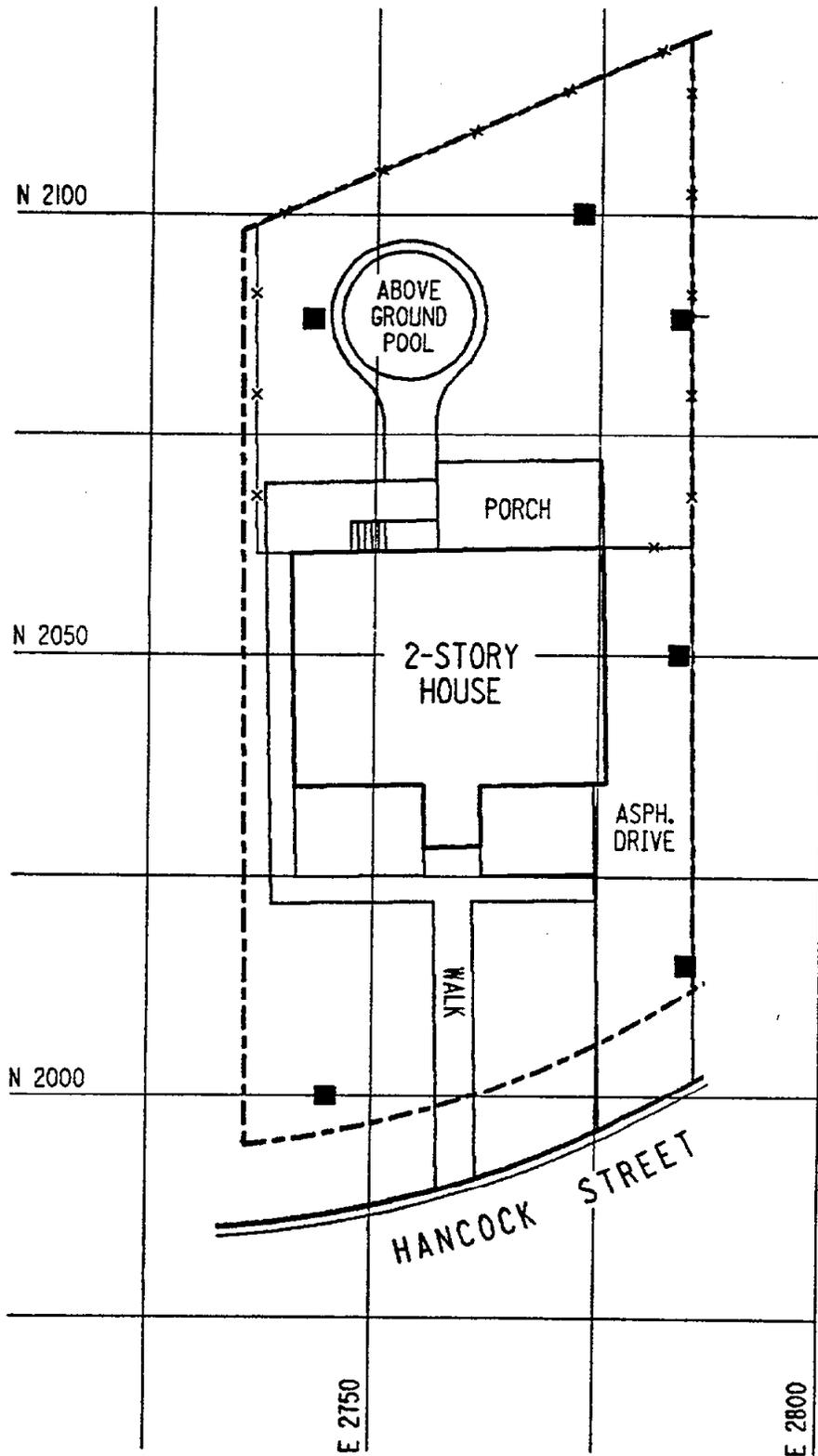


FIGURE 4-3 GAMMA EXPOSURE RATE MEASUREMENT LOCATIONS AT 5 HANCOCK STREET

## 5.0 CHARACTERIZATION RESULTS

Radiological characterization results are presented in this section. The data included represent exterior surface and subsurface radiation measurements and interior radiation measurements.

### 5.1 FIELD RADIOLOGICAL CHARACTERIZATION

Near-surface gamma radiation measurements on the property ranged from 3,000 cpm to approximately 10,000 cpm. The average background level for this area is 5,000 cpm. A measurement of 11,000 cpm is approximately equal to the DOE guideline for thorium-232 of 5 pCi/g above background for surface soil contamination. Using this correlation, the near-surface gamma measurements were used to determine the extent of surface contamination and the basis for selecting the locations of soil samples. No areas of surface contamination were indicated by near-surface gamma measurements.

Surface soil samples [depths from 0.0 to 15.2 cm (0.5 in.)] were taken at nine locations on the property (Figure 4-2). These samples were analyzed for thorium-232, uranium-238, and radium-226. The concentrations in these samples ranged from 2.5 to less than 13.8 pCi/g for uranium-238, from 1.1 to 5.8 pCi/g for thorium-232, and from 0.9 to 2.9 pCi/g for radium-226. Analytical results for surface soils are provided in Table 5-1; these data showed concentrations of thorium-232 in excess of DOE guidelines (5 pCi/g plus background of 1 pCi/g for surface soils) with a maximum concentration of 5.8 pCi/g. Use of the "less than" (<) notation in reporting results indicates that the radionuclide was not present in concentrations that are quantitative with the instruments and techniques used. The

"less than" value represents the lower bound of the quantitative capacity of the instrument and technique used. The "less than" value is based on various factors, including the volume, size, and weight of the sample; the type of detector used; the counting time; and the background count rate. The actual concentration of the radionuclide is less than the value indicated. In addition, since radioactive decay is a random process, a correlation between the rate of disintegration and a given radionuclide concentration cannot be precisely established. For this reason, the exact concentration of the radionuclide cannot be determined. As such, each value that can be quantitatively determined has an associated uncertainty term ( $\pm$ ), which represents the amount by which the actual concentration can be expected to differ from the value given in the table. The uncertainty term has an associated confidence level of 95 percent.

Thorium-232, the primary contaminant at the site, is the radionuclide most likely to exceed a specific DOE guideline in soil. Parameters for soil sample analysis were selected to ensure that the thorium-232 would be detected and measured at concentrations well below the lower guideline value of 5 pCi/g in excess of background level. Radionuclides of the uranium series, specifically uranium-238 and radium-226, are also potential contaminants but at lower concentrations than thorium-232. Therefore, these radionuclides (considered secondary contaminants) would not be present in concentrations in excess of guidelines unless thorium-232 was also present in concentrations in excess of its guideline level. Parameters selected for the thorium-232 analyses also provide detection sensitivities for uranium-238 and radium-226 that demonstrate that concentrations of these radionuclides are below guidelines. However, because of the relatively low gamma photon abundance of uranium-238, many of the uranium-238 concentrations were below the detection

sensitivity of the analytical procedure; these concentrations are reported in the data tables as "less than" values. To obtain more sensitive readings for the uranium-238 radionuclide with these analytical methods, much longer instrument counting times would be required than were necessary for analysis of thorium-232, the primary contaminant.

Analytical results for subsurface soil samples are given in Table 5-1, and gamma logging data are given in Table 5-2. The results in Table 5-2 showed a range from 8,000 cpm to 65,000 cpm. A measurement of 40,000 cpm is approximately equal to the DOE guideline for subsurface contamination of 15 pCi/g. Analyses of subsurface soil samples [taken at depths from 15.2 cm (0.5 in.) to the bottom of the hole when using the split-spoon sampler] indicated uranium-238 concentrations ranging from 1.0 to less than 13.3 pCi/g, thorium-232 concentrations ranging from 1.0 to 7.4 pCi/g, and radium-226 concentrations ranging from 0.7 to 1.7 pCi/g.

On the basis of near-surface gamma radiation measurements, surface and subsurface soil sample analyses, and downhole gamma logging, contamination on this property is believed to consist primarily of subsurface contamination at depths ranging from 0.30 m (1.0 ft) to 0.76 m (2.5 ft). The areas of subsurface contamination are shown in Figure 5-1. The subsurface contamination appears to extend beneath the residence as well as beneath an above-ground pool in the backyard.

It is apparent from review of historical documentation (e.g., aerial photographs of the area, interviews with local residents, and previous radiological surveys) that the subsurface contamination on this property lies along the

former channel of Lodi Brook and its associated floodplain. The contamination on this property is similar to contamination found on residential properties in close proximity to this property. It has been established that the Lodi Brook channel through these neighboring properties once occupied locations connecting to those where stream sediments were found at 5 Hancock Street. Thus, the elevated gamma readings shown on gamma logs from boreholes drilled on this property serve as further indication of the suspected mechanism of transport for radiological contamination (i.e., stream deposition from Lodi Brook).

The vertical and horizontal limits of contamination as determined by this characterization effort are being evaluated to determine the volume of contaminated material that will require remedial action. To develop this estimate, BNI will consider the location of the contamination, construction techniques, and safety procedures.

## 5.2 BUILDING RADIOLOGICAL CHARACTERIZATION

Results of indoor radon measurements made using the Tedlar bag method indicated concentrations of less than 0.2 and 0.4 pCi/L, respectively. These measurements were substantially less than the applicable DOE guideline of 3.0 pCi/L above background (Ref. 10).

Results of two measurements for radon daughters ranged from 0.0005 to 0.003 WL. These results were substantially less than the applicable generic guideline detailed in the Code of Federal Regulations, 40 CFR 192 (Ref. 10), which states that an annual average (or equivalent) radon decay product concentration not exceed 0.02 WL.

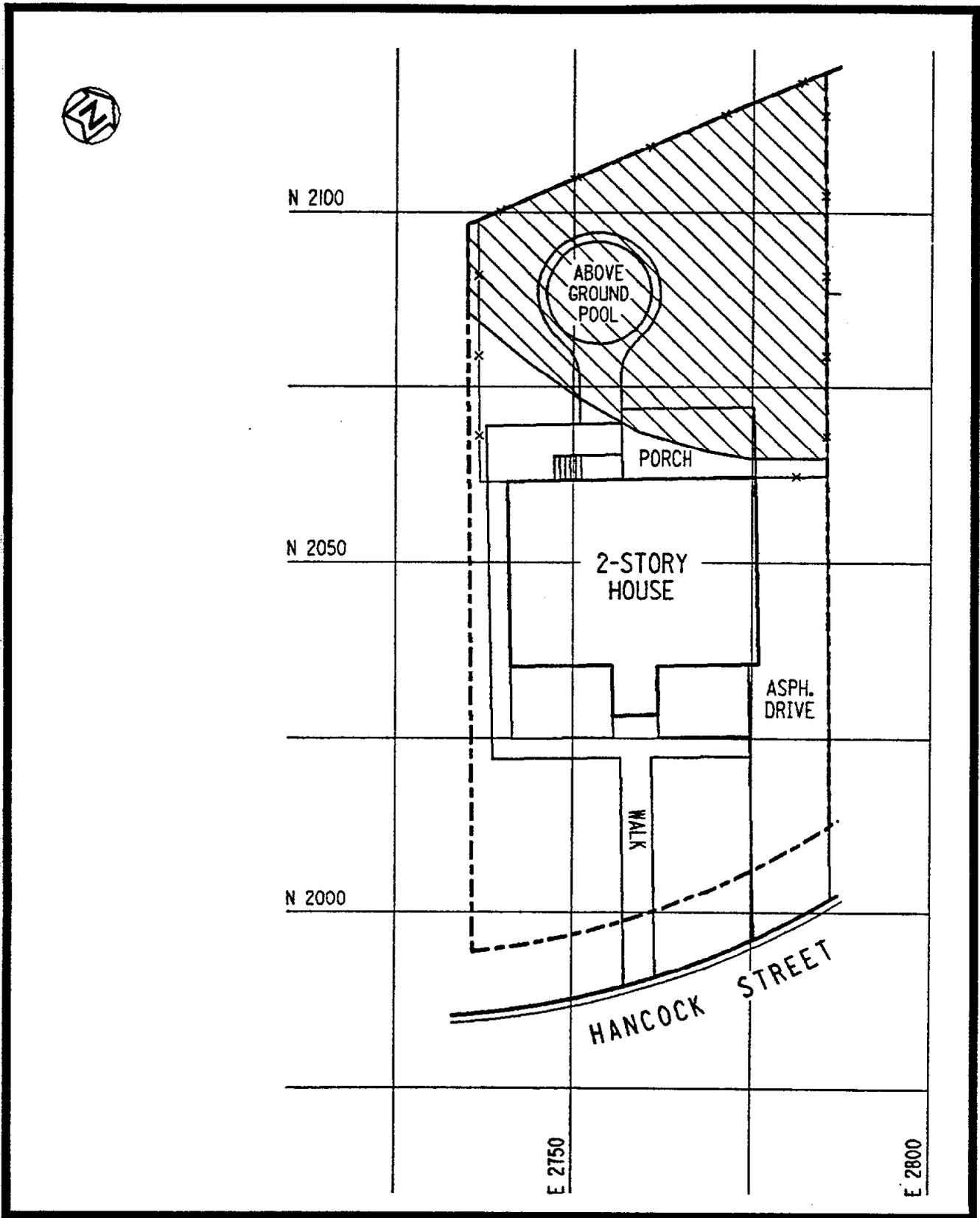


FIGURE 5-1 AREAS OF SUBSURFACE CONTAMINATION AT 5 HANCOCK STREET

Results of measurements for thoron daughters ranged from 0.007 to 0.003 WL. The generic guideline is more restrictive for radon-222 (radon) than for radon-220 (thoron) according to the National Council on Radiological Protection [see NCRP Report No. 50 (Ref. 11), which was used as the guideline for thoron daughter measurements].

Exterior gamma radiation exposure rate measurements ranged from 9 to 13  $\mu\text{R}/\text{h}$ , including background. These results can be found in Table 5-3). Assuming the resident spends 36 hours per week for 52 weeks per year (1,872 hours or 8 hours per day for 2 days per week and 4 hours day for 5 days per week) in the yard, the average exterior exposure rate of 11  $\mu\text{R}/\text{h}$  would result in a yearly dose of 4 mrem above background (after subtracting average background of 9  $\mu\text{R}/\text{h}$ ; Ref. 12).

The indoor exposure rate measurement was 6  $\mu\text{R}/\text{h}$ , including background. The indoor exposure rate does not exceed average background (Table 5-3). For comparison, the DOE guideline for indoor exposure rate is 20  $\mu\text{R}/\text{h}$ .

Based on the above information, the exposure rates and doses at this property are within DOE guidelines. Further, it should be emphasized that natural background exposure rates vary widely across the United States and are often significantly higher than average background for this area.

TABLE 5-1

## SURFACE AND SUBSURFACE RADIONUCLIDE CONCENTRATIONS IN SOIL

## FOR 5 HANCOCK STREET

Page 1 of 2

<u>Coordinates<sup>a</sup></u>		Depth (ft)	<u>Concentration (pCi/g <math>\pm</math> 2 sigma)</u>		
East	North		Uranium-238	Radium-226	Thorium-232
2736	2035	0.0 - 0.5	< 8.8	<1.4	2.0 $\pm$ 0.6
2736	2035	0.5 - 1.0	<10.4	0.8 $\pm$ 0.6	1.8 $\pm$ 0.8
2740	2092	0.0 - 0.5	< 3.0	< 1.0	1.3 $\pm$ 0.2
2740	2092	0.5 - 1.0	< 3.0	0.9 $\pm$ 0.2	1.5 $\pm$ 0.7
2740	2092	5.5 - 6.0	2.4 $\pm$ 1.7	< 1.0	1.8 $\pm$ 0.5
2742	2070	0.0 - 0.5	<10.5	1.3 $\pm$ 0.5	2.3 $\pm$ 0.5
2742	2070	0.5 - 1.0	< 8.9	< 1.2	1.7 $\pm$ 0.8
2744	2017	0.0 - 0.5	<10.5	< 1.5	< 3.2
2744	2017	0.5 - 1.0	< 8.3	< 1.2	1.4 $\pm$ 1.3
2763	2095	0.0 - 0.5	2.5 $\pm$ 0.5	0.8 $\pm$ 0.1	1.1 $\pm$ 0.1
2763	2095	0.5 - 1.0	1.0 $\pm$ 0.3	0.7 $\pm$ 0.1	1.0 $\pm$ 0.1
2763	2095	1.0 - 1.5	2.1 $\pm$ 1.8	1.0 $\pm$ 0.1	2.1 $\pm$ 0.7
2763	2095	1.5 - 2.0	< 4.0	1.3 $\pm$ 0.1	7.4 $\pm$ 0.8
2763	2095	2.0 - 2.5	< 3.0	0.8 $\pm$ 0.1	1.1 $\pm$ 0.1
2763	2095	2.5 - 3.0	2.6 $\pm$ 2.3	1.1 $\pm$ 0.1	5.6 $\pm$ 0.7
2763	2095	4.0 - 4.5	< 3.0	1.7 $\pm$ 0.1	1.8 $\pm$ 0.7
2763	2095	4.5 - 5.0	1.5 $\pm$ 1.1	0.9 $\pm$ 0.3	1.2 $\pm$ 0.3
2763	2095	6.0 - 6.5	3.6 $\pm$ 2.1	1.1 $\pm$ 0.5	1.4 $\pm$ 0.7
2763	2095	6.5 - 7.0	< 2.0	0.9 $\pm$ 0.1	1.2 $\pm$ 0.2
2763	2095	7.0 - 7.5	< 3.0	< 1.0	1.1 $\pm$ 0.4

TABLE 5-1  
(continued)

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<u>Coordinates<sup>a</sup></u>		<u>Depth (ft)</u>	<u>Concentration (pCi/g <math>\pm</math> 2 sigma)</u>		
<u>East</u>	<u>North</u>		<u>Uranium-238</u>	<u>Radium-226</u>	<u>Thorium-232</u>
2769	2012	0.0 - 0.5	< 9.1	< 1.3	1.9 $\pm$ 1.0
2769	2012	0.5 - 1.0	<10.7	1.4 $\pm$ 0.5	< 3.7
2770	2073	0.0 - 0.5	<10.1	1.0 $\pm$ 0.4	< 2.9
2770	2073	0.5 - 1.0	<13.3	1.5 $\pm$ 0.7	4.0 $\pm$ 1.2
2777	2058	0.0 - 0.5	< 8.5	1.3 $\pm$ 0.3	2.8 $\pm$ 0.04
2777	2058	0.5 - 1.0	<11.0	1.6 $\pm$ 0.2	3.3 $\pm$ 0.8
2783	2095	0.0 - 0.5	<13.8	2.9 $\pm$ 0.6	5.8 $\pm$ 0.9
2783	2095	0.5 - 1.0	<11.9	0.7 $\pm$ 0.3	5.2 $\pm$ 1.5

<sup>a</sup>Sampling locations are shown in Figure 4-2.

TABLE 5-2

## DOWNHOLE GAMMA LOGGING RESULTS

FOR 5 HANCOCK STREET

Page 1 of 4

Coordinates <sup>a</sup>		Depth <sup>b</sup> (ft)	Count Rate <sup>c</sup> (cpm)
East	North		
<u>Borehole 609R<sup>d</sup></u>			
2736	2035	0.5	14000
2736	2035	1.0	13000
2736	2035	1.5	13000
2736	2035	2.0	12000
2736	2035	2.5	9000
2736	2035	3.0	9000
2736	2035	3.5	10000
2736	2035	4.0	10000
2736	2035	4.5	12000
2736	2035	5.0	11000
<u>Borehole 2049R</u>			
2740	2092	0.5	17000
2740	2092	1.0	39000
2740	2092	1.5	55000
2740	2092	2.0	46000
2740	2092	2.5	17000
2740	2092	3.0	13000
2740	2092	3.5	10000
2740	2092	4.0	10000
2740	2092	4.5	10000
2740	2092	5.0	11000
2740	2092	5.5	10000
<u>Borehole 593R<sup>d</sup></u>			
2742	2070	0.5	12000
2742	2070	1.0	25000
2742	2070	1.5	27000
2742	2070	2.0	16000
2742	2070	2.5	14000
2742	2070	3.0	13000
2742	2070	3.5	12000
2742	2070	4.0	12000
2742	2070	4.5	12000
2742	2070	5.0	11000
2742	2070	5.5	10000
2742	2070	6.0	9000

TABLE 5-2  
(continued)

Page 2 of 4

Coordinates <sup>a</sup>		Depth <sup>b</sup> (ft)	Count Rate <sup>c</sup> (cpm)
East	North		
<u>Borehole 589R<sup>d</sup></u>			
2744	2017	0.5	13000
2744	2017	1.0	13000
2744	2017	1.5	12000
2744	2017	2.0	13000
2744	2017	2.5	14000
2744	2017	3.0	13000
2744	2017	3.5	12000
2744	2017	4.0	11000
2744	2017	4.5	10000
2744	2017	5.0	9000
2744	2017	5.5	7000
2744	2017	6.0	7000
2744	2017	6.5	8000
2744	2017	7.0	7000
<u>Borehole 2007R<sup>d</sup></u>			
2763	2095	0.5	13000
2763	2095	1.0	27000
2763	2095	1.5	36000
2763	2095	2.0	25000
2763	2095	2.5	17000
2763	2095	3.0	15000
2763	2095	3.5	16000
2763	2095	4.0	13000
2763	2095	4.5	12000
2763	2095	5.0	12000
2763	2095	5.5	14000
2763	2095	6.0	14000
2763	2095	6.5	14000
2763	2095	7.0	12000
<u>Borehole 588R<sup>d</sup></u>			
2769	2012	0.5	11000
2769	2012	1.0	13000
2769	2012	1.5	15000
2769	2012	2.0	15000
2769	2012	2.5	15000
2769	2012	3.0	21000
2769	2012	3.5	20000
2769	2012	4.0	17000

TABLE 5-2

(continued)

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<u>Coordinates<sup>a</sup></u>		<u>Depth<sup>b</sup></u> (ft)	<u>Count Rate<sup>c</sup></u> (cpm)
<u>East</u>	<u>North</u>		
<u>Borehole 588R (continued)<sup>d</sup></u>			
2769	2012	4.5	12000
2769	2012	5.0	12000
2769	2012	5.5	13000
2769	2012	6.0	12000
2769	2012	6.5	16000
<u>Borehole 591R<sup>d</sup></u>			
2770	2073	0.5	15000
2770	2073	1.0	15000
2770	2073	1.5	38000
2770	2073	2.0	53000
2770	2073	2.5	28000
2770	2073	3.0	22000
2770	2073	3.5	23000
2770	2073	4.0	19000
2770	2073	4.5	16000
2770	2073	5.0	10000
2770	2073	5.5	9000
2770	2073	6.0	10000
<u>Borehole 590R<sup>d</sup></u>			
2777	2058	0.5	10000
2777	2058	1.0	13000
2777	2058	1.5	15000
2777	2058	2.0	22000
2777	2058	2.5	22000
2777	2058	3.0	21000
2777	2058	3.5	22000
2777	2058	4.0	20000
2777	2058	4.5	16000
2777	2058	5.0	13000
2777	2058	5.5	12000
2777	2058	6.0	11000
2777	2058	6.5	11000
<u>Borehole 592R<sup>d</sup></u>			
2783	2095	0.5	12000
2783	2095	1.0	16000
2783	2095	1.5	17000

TABLE 5-2  
(continued)

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Coordinates <sup>a</sup>		Depth <sup>b</sup>	Count Rate <sup>c</sup>
East	North	(ft)	(cpm)
<u>Borehole 592R (continued)<sup>d</sup></u>			
2783	2095	2.0	65000
2783	2095	2.5	50000
2783	2095	3.0	25000
2783	2095	3.5	22000
2783	2095	4.0	21000
2783	2095	4.5	14000
2783	2095	5.0	13000
2783	2095	5.5	14000

<sup>a</sup>Borehole locations are shown in Figure 4-1.

<sup>b</sup>The variations in depths of boreholes and corresponding results given in this table are based on the boreholes penetrating the contamination or the drill reaching refusal.

<sup>c</sup>Instrument used was 5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide gamma scintillation detector.

<sup>d</sup>Bottom of borehole collapsed.

TABLE 5-3  
 GAMMA RADIATION EXPOSURE RATES  
 FOR 5 HANCOCK STREET

Coordinates <sup>a</sup>		Rate <sup>b</sup> ( $\mu$ R/h)
East	North	
2743	2088	10
2745	2000	10
2773	2100	12
2785	2015	10
2788	2050	9
2788	2088	13
Interior of Residence		6

<sup>a</sup>Measurement locations are shown in Figure 4-3.

<sup>b</sup>Measurements include background.

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**APPENDIX A**  
**GEOLOGIC DRILL LOGS FOR 5 HANCOCK STREET**

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.			
5 Hancock St. (LODI)				FUSRAP		14501-138	1 OF 1	609R			
SITE			COORDINATES			ANGLE FROM HORIZ		BEARING			
5 Hancock St. (LODI)			N 2,035 E 2,736			Vertical		-----			
BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH				
11-21-86	11-21-86	MORETRENCH	B&S Little Beaver	4"	8.5		8.5				
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER		DEPTH/EL. TOP OF ROCK			
/						7.0/ 11-21-86		/			
SAMPLE HAMMER WEIGHT/FALL			CASING LEFT IN HOLE: DIA./LENGTH		LOGGED BY:						
N/A			NONE		D. McGRANE <i>JAL</i>						
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMP. REC. CORE REC.	SAMP. BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS		ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.						
							5			<p>0.0 - 8.5 ft. <b>Silty SAND (SM)</b>. Fill (0.0-6.0 ft.) and indigenous material (6.0-8.5 ft.) Color stratified. Fine- to medium-grained with a few pieces of rounded to angular gravel (and occasional cobbles) of various lithologies in the fill material. Soft, unconsolidated (loose), sometimes clayey (SC-OH). Moist to saturated at 7.0 ft.</p> <p>0.0-0.3 ft. Moderate brown (5YR3/4). Numerous grass roots and organics.</p> <p>0.3-6.0 ft. Dark reddish brown (10R3/4).</p> <p>6.0-7.0 ft. Moderate brown. May be buried upper soil horizon.</p> <p>7.0-8.5 ft. Dark yellowish brown (10YR4/2). May be decomposed sandstone.</p> <p>Bottom of borehole at 8.5 ft. Auger spoils were replaced in the hole, 11-21-86.</p>	<p>Borehole drilled 0.0-8.5 ft. using 4" solid-stem augers.</p> <p>Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.</p> <p>7.0 ft. ground water observed.</p>
											Description and classification of soil samples by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

5 Hancock St. (LODI)

HOLE NO. 609R

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.			
				FUSRAP		14501-138	1 OF 1	2049R			
SITE			COORDINATES			ANGLE FROM HORIZ BEARING					
5 Hancock St. (LODI)			N 2,092 E 2,740			Vertical -----					
BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL		SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH			
11-15-88	11-15-88	EMPIRE SOILS	Tripod & Hammer		3"	6.0		6.0			
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER		DEPTH/EL. TOP OF ROCK			
/			3			/		/			
SAMPLE HAMMER WEIGHT/FALL		CASING LEFT IN HOLE: DIA./LENGTH		LOGGED BY:							
140 lb. / 12 in.		NONE		J. LORD 							
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMP. REC. CORE REC.	SAMPLE BLOWS "IN" X CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.					
SS	2.0	0.8	9-11 17-25						0.0 - 0.5 Ft. <b>TOPSOIL</b> . Moderate brown (5YR3/4). Dry, loose, silty sand topsoil with roots, grass, and organic flecks.	0-6 ft. advanced using 3 in. i.d. split spoon samplers. Sampled and gamma-scanned by TMA-Eberline, Corp.	
SS	2.0	0.0	27-22 23-25						0.5 - 1.0 Ft. <b>Silty SAND (SM)</b> . Reddish brown (10R4/6). Moderately compacted, stiff, slightly moist. Poorly sorted with some gravel.		
SS	2.0	0.5	15-18 21-30				5		1.0 - 5.5 Ft. <b>NO RECOVERY</b> .		
									5.5 - 6.0 Ft. <b>Silty SAND (SM)</b> . Reddish brown (10R4/6) bulk color. Mixed minor sworls of other colors. Moderately compacted, slightly moist. Poorly sorted coarse-grained sand with Brunswick SS gravel. Possible fill material.	No ground water detected in hole.	
Bottom of borehole at 6.0 Ft. Borehole backfilled with dry grout to 6" below surface, clean sod to the surface, 11/15/88.										Top of undisturbed soil not penetrated?	
Description and classification of soils by visual examination of samples.											

SS = SPLIT SPOON; ST = SHELBY TUBE;  
D = DENNISON; P = PITCHER; O = OTHER

SITE  
5 Hancock St. (LODI)

HOLE NO.  
2049R

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.						
5 Hancock St. (LODI)				N 2,070 E 2,742		14501-138	1 OF 1	593R						
BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL		SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH						
11-18-86	11-18-86	MORETRENCH	B&S Little Beaver		4"	9.0		9.0						
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER		DEPTH/EL. TOP OF ROCK						
/						8.0/ 11-18-86		/						
SAMPLE HAMMER WEIGHT/FALL		CASING LEFT IN HOLE: DIA./LENGTH			LOGGED BY:									
N/A		NONE			D. McGRANE <i>gpr</i>									
SAMP. TYPE AND DIAM.	SAMP. ADJ. LEN. CORE	SAMP. REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.		
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.								
											<p>0.0 - 9.0 ft. Silty SAND (SM). Fill (0.0-6.0) and indigenous material (6.0-9.0) Color stratified. Fine- to medium-grained with a few pieces of rounded to angular gravel (and occasional cobbles) of various lithologies in the fill material. Soft, unconsolidated (loose), sometimes clayey (SC-OH). Moist to saturated at 8.0 ft.</p> <p>0.0-0.3 ft. Moderate brown (5YR3/4). Numerous grass roots and organics.</p> <p>0.3-3.0 ft. Dark reddish brown (10R3/4), mottled moderate brown.</p> <p>3.0-6.0 ft. Dark yellowish brown (10YR4/2); piece of plastic (5.0 ft.).</p> <p>6.0-9.0 ft. Dark yellowish brown (10YR4/2). May be decomposed sandstone.</p> <p>Bottom of borehole at 9.0 ft. Auger spoils were replaced in the hole, 11-18-86.</p>	<p>Borehole drilled 0.0-9.0 ft. using 4" solid-stem augers.</p> <p>Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.</p> <p>8.0 ft. ground water observed.</p>		
SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER											SITE	5 Hancock St. (LODI)	HOLE NO.	593R

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.				
5 Hancock St. (LODI)				N 2,017 E 2,744		14501-138	1 OF 1	589R				
BEGUN		COMPLETED	DRILLER	DRILL MAKE AND MODEL		SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH			
11-18-86		11-18-86	MORETRENCH	B&S Little Beaver		4"	12.0		12.0			
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER		DEPTH/EL. TOP OF ROCK				
/						8.0/ 11-18-86		/				
SAMPLE HAMMER WEIGHT/FALL			CASING LEFT IN HOLE: DIA./LENGTH			LOGGED BY:						
N/A			NONE			D. McGRANE <i>DM</i>						
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN. CORE	SAMP. REC. CORE REC.	SAMPLE BLOWS "IN" % CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.						
											<p>0.0 - 12.0 ft. <u>Silty SAND (SM)</u>. Fill (0.0-8.0) and indigenous material (8.0-12.0) Color stratified. Fine- to medium-grained with a few pieces of rounded to angular gravel (and occasional cobbles) of various lithologies in the fill material. Soft, unconsolidated (loose), sometimes clayey (SC-OH). Moist to saturated at 8.0 ft.</p> <p>0.0-0.3 ft. Moderate brown (5YR3/4). Numerous grass roots and organics.</p> <p>0.3-8.0 ft. Dark reddish brown (10R3/4).</p> <p>8.0-12.0 ft. Dark yellowish brown (10YR4/2). May be decomposed sandstone.</p>	<p>Borehole drilled 0.0-12.0 ft. using 4" solid-stem augers.</p> <p>Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.</p> <p>8.0 ft. ground water observed.</p>
											<p>Bottom of borehole at 12.0 ft. Auger spoils were replaced in the hole, 11-18-86.</p>	<p>Description and classification of soil samples by visual examination.</p>
SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER										SITE		HOLE NO.
5 Hancock St. (LODI)										589R		

GEOLOGIC DRILL LOG				PROJECT	JOB NO.	SHEET NO.	HOLE NO.					
				FUSRAP	14501-138	1 OF 1	2007R					
SITE			COORDINATES			ANGLE FROM HORIZ	BEARING					
5 Hancock St. (LODI)			N 2,905 E 2,763			Vertical	-----					
BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH					
10-5-88	10-5-88	EMPIRE SOILS	Tripod & Hammer	3"	10.0		10.0					
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK					
			5									
SAMPLE HAMMER WEIGHT/FALL		CASING LEFT IN HOLE: DIA./LENGTH		LOGGED BY:								
140 Lb. / 12 in.		NONE		J. LORD								
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN. CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS			ELEU.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.						
SS	2.0	1.9	7-14 29-33								0.0 - 1.0 Ft. <b>TOPSOIL</b> . Moderate brown (5YR5/4). Dry, loose, silty sand topsoil with roots, grass, and organic flecks.	0-10 ft. advanced using 3 in. i.d. split spoon samplers. Sampled and gamma-scanned by TMA-Eberline, Corp.  No ground water detected.  Top of undisturbed soil not confirmed.  Elevated counts between 1.0-2.5 Ft.
SS	2.0	1.0	32-37 43-17							1.0 - 3.0 Ft. <b>Silty SAND (SM)</b> . Reddish brown (10R4/6). Moderately compacted, stiff, slightly moist. Poorly sorted with some gravel.		
SS	2.0	1.0	52-22 27-17				5			3.0 - 5.5 Ft. <b>FILL?</b> . Little to no recovery. The little that is recovered is asphalt-like, dry, sandy material.		
SS	2.0	1.2	28-20 46-47							5.5 - 8.0 Ft. <b>Silty SAND (SM)</b> . Reddish brown (10R4/6) bulk color. Mixed minor swirls of other colors. Moderately compacted, stiff, slightly moist. Poorly sorted with some gravel and chunks of Brunswick SS. Possible fill material.		
SS	2.0	0.0	53-23 30-19				10			8.0 - 10.0 Ft. <b>NO RECOVERY</b> .		
Bottom of borehole at 10.0 Ft. Borehole backfilled with dry grout to 6" below surface, clean sod to the surface, 10/5/88.												
SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER SITE: <b>5 Hancock St. (LODI)</b>												HOLE NO. <b>2007R</b>

GEOLOGIC DRILL LOG				PROJECT		JOB NO.		SHEET NO.		HOLE NO.		
5 Hancock St. (LODI)				N 2,012 E 2,769		14501-138		1 OF 1		588R		
BEGUN			COMPLETED			DRILLER			DRILL MAKE AND MODEL			
11-18-86			11-18-86			MORETRENCH			B&S Little Beaver			
CORE RECOVERY (FT./%)			CORE BOXES/SAMPLES			EL. TOP CASING			GROUND EL.			
/			/			/			8.0/ 11-18-86			
SAMPLE HAMMER WEIGHT/FALL				CASING LEFT IN HOLE: DIA./LENGTH				LOGGED BY:				
N/A				NONE				D. McGRANE <i>JAR</i>				
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMP. REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.						
										0.0 - 9.0 ft. Silty SAND (SM). Fill (0.0-5.0) and indigenous material (5.0-9.0) Color stratified. Fine- to medium-grained with a few pieces of rounded to angular gravel (and occasional cobbles) of various lithologies in the fill material. Soft, unconsolidated (loose), sometimes clayey (SC-OH). Moist to saturated at 8.0 ft.  0.0-0.3 ft. Moderate brown (5YR3/4). Numerous grass roots and organics.  0.3-5.0 ft. Dark reddish brown (10R3/4).  3.0-9.0 ft. Moderate brown. May be buried upper soil horizons.	Borehole drilled 0.0-9.0 ft. using 4" solid-stem augers.  Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.  8.0 ft. ground water observed.	
										Bottom of borehole at 9.0 ft. Auger spoils were replaced in the hole, 11-18-86.	Description and classification of soil samples by visual examination.	

SS = SPLIT SPOON; ST = SHELBY TUBE; SITE  
 D = DENNISON; P = PITCHER; O = OTHER

5 Hancock St. (LODI)

HOLE NO. 588R

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.					
5 Hancock St. (LODI)				COORDINATES		FUSRAP	14501-138 1 OF 1	591R					
BEGUN		COMPLETED	DRILLER	DRILL MAKE AND MODEL		SIZE	OVERBURDEN	ANGLE FROM HORIZ	BEARING				
11-18-86		11-18-86	MORETRENCH	B&S Little Beaver		4"	9.0	Vertical	-----				
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER		DEPTH/EL. TOP OF ROCK					
/						8.0/ 11-18-86		/					
SAMPLE HAMMER WEIGHT/FALL			CASING LEFT IN HOLE: DIA./LENGTH			LOGGED BY:							
N/A			NONE			D. McGRANE <i>DMG</i>							
SAMP. TYPE AND DIAM.	SAMP. ADU. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.	
				LOSS IN G.P.N	PRESS. P.S.I.	TIME IN MIN.							
											<p>0.0 - 3.0 ft. <b>Silty SAND (SM)</b>. Fill material. Multicolored. Fine- to medium-grained with few to numerous pieces of rounded to angular gravel (and occasional cobbles) of various lithologies. Soft, unconsolidated (loose), moist.</p> <p>0.0-0.3 ft. Moderate brown (5YR3/4). Numerous roots and organics.</p> <p>0.3-3.0 ft. Dark reddish brown (10R3/4) with mottled moderate brown.</p> <p>3.0 - 6.0 ft. <b>SAND (PT)</b>. Coal ash fill. Black (N1). Fine- to coarse-grained, soft, very low density, unconsolidated (loose), moist.</p> <p>6.0 - 9.0 ft. <b>Silty SAND (SM-SC)</b>. Indigenous soil. Fine- to medium-grained. Soft, unconsolidated (loose). Moist to saturated at 8.0 ft.</p> <p>6.0-8.0 ft. Moderate brown. May be buried upper soil horizon.</p> <p>8.0-9.0 ft. Dark yellowish brown (10YR4/2). May be decomposed sandstone.</p> <p>Bottom of borehole at 9.0 ft. Auger spoils were replaced in the hole, 11-18-86.</p>	<p>Borehole drilled 0.0-9.0 ft. using 4" solid-stem augers.</p> <p>Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.</p> <p>8.0 ft. ground water observed.</p> <p>Description and classification of soil samples by visual examination.</p>	
SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER										SITE		HOLE NO.	
5 Hancock St. (LODI)										591R			

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.			
5 Hancock St. (LODI)				COORDINATES		14501-138	1 OF 1	590R			
N 2,058 E 2,777				ANGLE FROM HORIZ		Vertical		-----			
BEGUN	COMPLETED	DRILLER		DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH			
11-18-86	11-18-86	MORETRENCH		B&S Little Beaver	4"	9.0		9.0			
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER		DEPTH/EL. TOP OF ROCK			
/						7.0/ 11-18-86		/			
SAMPLE HAMMER WEIGHT/FALL		CASING LEFT IN HOLE: DIA./LENGTH		LOGGED BY:							
N/A		NONE		D. McGRANE 							
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN. CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.					
									<p>0.0 - 4.0 ft. <u>Silty SAND (SM)</u>. Fill material. Multicolored. Fine- to medium-grained with few to numerous pieces of rounded to angular gravel (and occasional cobbles) of various lithologies. Soft, unconsolidated (loose), moist.</p> <p>0.0-0.3 ft. Moderate brown (5YR3/4). Numerous grass roots and organics.</p> <p>0.3-4.0 ft. Dark reddish brown (10R3/4).</p> <p>4.0 - 7.0 ft. <u>SAND (PT)</u>. Coal ash fill. Black (N1). Fine- to coarse-grained. Soft, very low density, unconsolidated (loose). Moist to saturated at 7.0 ft.</p> <p>7.0 - 9.0 ft. <u>Silty SAND (SM)</u>. Dark yellowish brown (10YR4/2). Fine- to medium-grained. Soft, unconsolidated (loose), saturated. May be decomposed sandstone.</p> <p>Bottom of borehole at 9.0 ft. Auger spoils were replaced in the hole, 11-18-86.</p>	<p>Borehole drilled 0.0-9.0 ft. using 4" solid-stem augers.</p> <p>Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.</p> <p>7.0 ft. ground water observed.</p>	
										Description and classification of soil samples by visual examination.	

SS = SPLIT SPOON; ST = SHELBY TUBE;  
D = DENNISON; P = PITCHER; O = OTHER

SITE  
**5 Hancock St. (LODI)**

HOLE NO.  
**590R**

GEOLOGIC DRILL LOG				PROJECT		JOB NO.	SHEET NO.	HOLE NO.				
5 Hancock St. (LODI)				COORDINATES		14501-138	1 OF 1	592R				
N 2,095 E 2,783				ANGLE FROM HORIZ		Vertical		-----				
BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH					
11-18-86	11-18-86	MORETRENCH	B&S Little Beaver	4"	9.0		9.0					
CORE RECOVERY (FT./%)		CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK					
/							/					
SAMPLE HAMMER WEIGHT/FALL			CASING LEFT IN HOLE: DIA./LENGTH			LOGGED BY:						
N/A			NONE			D. McGRANE <i>gr</i>						
SAMP. TYPE AND DIAM.	SAMP. ADV. LEN. CORE	SAMP. REC. CORE REC.	SAMP. BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS			ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
				LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.						
											<p>0.0 - 3.0 ft. <u>Silty SAND (SM)</u>. Fill material. Multicolored. Fine- to medium-grained with few to numerous pieces of rounded to angular gravel (and occasional cobbles) of various lithologies. Soft, unconsolidated (loose), moist.</p> <p>0.0-3.0 ft. Moderate brown (5YR3/4). Numerous grass roots and organics (0.0-0.3 ft.).</p> <p>3.0 - 6.0 ft. <u>SAND (PT)</u>. Coal ash fill. Black (N1). Fine- to coarse-grained. Soft, very low density, unconsolidated (loose), moist.</p> <p>6.0 - 9.0 ft. <u>Silty SAND (SM)</u>. Indigenous soil. Fine- to medium-grained. Soft, unconsolidated (loose), moist.</p> <p>6.0-7.0 ft. Moderate brown; few cobbles. May be buried upper soil horizon.</p> <p>7.0-9.0 ft. Dark yellowish brown (10YR4/2). May be decomposed sandstone.</p> <p>Bottom of borehole at 9.0 ft. Auger spoils were replaced in the hole, 11-18-86.</p>	<p>Borehole drilled 0.0-9.0 ft. using 4" solid-stem augers.</p> <p>Site checked for radioactive contamination and hole gamma-logged by TMA-Eberline, Corp.</p> <p>No ground water observed.</p> <p>Description and classification of soil samples by visual examination.</p>

SS = SPLIT SPOON; ST = SHELBY TUBE; SITE  
 D = DENNISON; P = PITCHER; O = OTHER

5 Hancock St. (LODI)

HOLE NO.  
592R